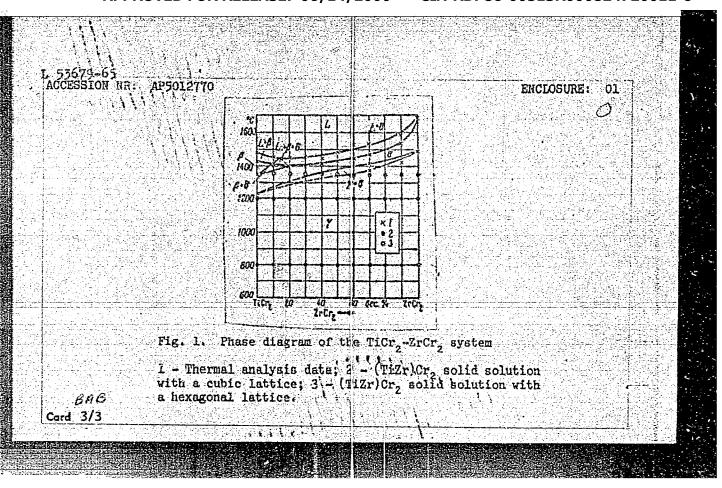
| <u>. 53679-65</u> | b)/EWA(c) Pu-4 IJP(c) JD/WW/JG |
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| ACCESSION NR: AP5012770 | UR/0020/65/161/006/1378/1361 |
| AUTHOR: Kornilov, I. I.; Budberg, P. B.; St | gákhova, K. I.; Alisova, S. P. |
| | |
| TITLE: Phase diagram of the TiCr2-ZrCr2 sys | Lij65, 1378–138L |
| TOPIC TAGS: titanium chromium alloy, zircor alloy composition, alloy structure, alloy cr | |
| APSTRACT: The phase composition and microst and nine TiCr ₂ -ZrCr ₂ alloys containing from melted and homogenized at 1250—1300C for 50 | to to 90% TiCr, are and levitation |
| phase analysis. Thermal analysis showed the creased with increasing ZrCr2 content, e.g., ZrCr2, respectively. An analogous increase | at the alloy liquidus temperatures in- from 1480 to 1675C for pure TiCr2 and |
| phase diagram of the TiCr ₂ -ZrCr ₂ system (see obtained data is characterized by the format lutions between both the low-temperature and TiCr ₂ and ZrCr ₂ compounds. The appearance of | e Fig. 1 of the Enclosure) based on the thon of a continuous series of solid so- d the high-temperature modifications of |
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| 53679-65 CCESSION NR: AP5012770 L+β+6) regions in the T | iCr ₂ -rich alloys is e inary Ti-Cr system in | explained by the fact that the TiCr of the solid state. Orig. art. has: [MS] | 2 |
|---|---|--|---|
| 4 figures and 2 tables. | illurgii im. <u>A. A. B</u> | aykova (Institute of Metallurgy) SUB CODE: MM,SS | |
| SUBMITTED: 095v164 NO REF SOV: 006 | ENCL: 01 OTHER: 006 | ATD PRESS: 4011 | |
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| 5250-65 EWT(m)/EWP(w)/EWA(d)/EWP(t)/T/EWP(b)/EWP(z)/EWA(c) Pad IJP(c) ESSION NR: AP5013122 UR/0370/65/050/002/0175/0179 669.017.12 HOR: Kornilov, I. I.; Myasnikova, K. P. | |
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| ESSION NR: AP5013122 UR/0370/65/060/002/0175/0179 . | |
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| HOR: Kormilov, I. I.; Myasnikova, K. P. 28 | |
| HOR: Kornilov, I. I.; Myasnikova, K. P. 28 | |
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| LE: The phase diagram and some properties of nickel-rhodium alloys | |
| | |
| RCE: AN SSSR. Izvestiya. Metally, no. 2, 1965, 175-179 | |
| 一点,你就是一点,你就是你的,我们还是你是我的,我们就会是我的的女子就是她就能看了一个的女子,我们就是一个人,我们,我们也没有一点的。""这一个人,我们也没有 | |
| IC TAGS: nickel alloy, rhodium alloy, metal physical property, metal mechanic | cal |
| A struct A burge diagram | |
| IPACT: The phase diagram was determined | |
| FACT: The phase diagram was determined using thermal, microstructural and x-analysis. Electrical resistance, microstructural and x- | - , |
| analysis. Electrical resistance, microhardness and hardness at room and ele- id temperatures (up to 1273°K) were investigated. The phase diagram shows a | - |
| The series of solid solutions extending from the phase diagram shows a | |
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EVT(m)/EWP(t)/FTI SOURCE CODE: I.IP(c) ACC NR: AP5027845 UR/0020/65/165/001/0136/013 AUTHOR: Glazova, V. V.; Kornilov, I. I.; Modestova, V. N.; Tomashov, ORG: Institute of Metallurgy im. A. A. Baykov (Institut metallurgii); Institute of Physical Chemistry, AN SSSR (Institut fizicheskoy khimii AN SSSR) TITLE: Corrosion behavior in sulfuric acid solution of alloys of the titanium-oxygen system SOURCE: AN SSSR. Doklady, v. 165, no. 1, 1965, 136-139 TOPIC TAGS: titanium compound, titanium base alloy, corrosion resistance, electrode potential, sulfuric acid ABSTRACT: Titanium has a large affinity to oxygen and the presence of a Ti compound with oxygen decelerates corrosion considerably. It was of interest, therefore, to study the behavior of Ti alloys with oxygen. The Ti-O alloys were prepared in an arc furnace with a noncombustible W electrode in an Ar atmosphere. The initial materials were: Ti iodide (99.9% Ti) and Ti oxide (99.93% TiO2). The oxygen was added in the form of an alloy containing 15.8% oxygen and prepared by melting in the arc furnace tablets compressed from Ti and TiO2. The Ti-O alloys, containing 1, 5, 9, 10, 11, 12, 13, 15, 16, 17, 20, 25, and 36 at soxygen, were thus prepared. The study of corrosion resistance and stationary electrode potential of the Ti-O alloys was made in 40% and 70% $\rm H_2SO_{\Delta}$, i.e. under conditions of the strongest possible corresion of Ti. The curves Card 1/2 UDC: 620.197.3

"APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R000824720011-6

L 36924-66 EWT(m)/T/EWP(t)/ETI IJP(c) JD/JG ACC NR: AP6008497 SOURCE CODE: UR/0062/66/000/001/0008/0016

AUTHOR: Kornilov, I. I., Matveyeva, N. M.

《古代文学》,1985年1985年1985年1985年1985年1985

ORG: Institute of Metallurgy im. A. A. Baykov (Institut metallurgii)

TITLE: Investigation in metal chemistry. Communication 5. Interaction between intermetallic compounds

SOURCE: AN SSSR. Izvestiya. Seriya khimicheskaya, no. 1, 1966, 8-16

TOPIC TAGS: intermetallic compound, metal chemical analysis, solid solution

ABSTRACT: In this work the authors discuss the basic physicochemical factors determining the interactions between intermetallic compounds and cite their latest experimental data. Intermetallic compounds in equilibrium systems are treated as individual components. During their interaction continuous solid solutions, limited solid solutions, peritectic and eutectic mixtures, and ternary compounds or phases of a complex composition can form. In contrast to solid solutions of metals, the authors termed solid solutions on a base of metallic compounds intermetallic (metallide) solid solutions. Continuous or limited solid solutions of intermetallic compounds under certain conditions are formed between Kurnakov compounds, berthollide-type compounds, daltonide-type compounds, and compounds of the berthollide and daltonide types. The authors examined certain examples of the

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interaction between compounds from the data of their investigations, one of the first systems with a continuous solid solution of intermetallic compounds being the system consisting of the CrFe and VFe Kurnakov compounds. These compounds are formed in binary systems from continuous a-solid solutions of components upon a drop of temperature. Both compounds with respect both to chemical and to structural features satisfy the basic conditions for the formation of continuous solid solutions expressed by the author, i.c., that the compounds should have an identical type of crystal structure with similar values of the lattice parameters, similar type of chemical bond in the compounds, the presence in the compositions of these compounds of the atoms of elements (analogs) capable of being continuously replaced in the crystal lattice of the compounds, the presence in the compositions of two interacting compounds of atoms of the same element, and that the compound should have an identical stoichiometric composition. The intermetallic compounds have special, individual properties and play a most important role in the physicochemical and mechanical properties of metal alloys. They have an independent importance as the base for new inorganic materials with special physical properties. The properties of intermetallic compounds can be appreciably modified by their interaction with one another and by the formation of intermetallic solid solutions, eutectic mixtures, and complex multielement compounds. The level of the physicochemical and mechanical properties in intermetallic compound systems is appreciably higher than in simple metallic systems.

Card 2/3

KORNILOV, I.I.; CLGZOVA, V.V.

Studies in metal chemistry. Report No.6: Suboxides of transition metals. Izv.AN SSSR. Ser.khim. no.1:16-23 '66.

(MIRA 19:1)

1. Institut metallurgii im. A.A.Baykova. Submitted August 22, 1963.

Weing titanium in chemical machinery manufacture and principles of its alloying. Zashch. met. 2 no.1:25-31 Ja-F '66. (MIRA 19:1)

1. Institut metallurgii imeni A.A. Baykova, Moskva. Submitted March 11, 1965.

L 38971-56 ENI(m)/EWP(w)/T/EWP(t)/ETI IJP(c) JD/JG

ACC NR: AP6013367 SOURCE CODE: UR/0370/66/000/002/0137/0143

AUTHOR: Kornilov, I. I. (Moscow); Pylayeva, Ye. N. (Moscow); Volkova, M. A. (Moscow)

ORG: none

TITLE: Evaluation of the creep of alloys of the Ti-Al-V system by the bending method at elevated temperatures

SOURCE: AN SSSR. Izvestiya. Metally, no. 2, 1966, 137-143

TOPIC TAGS: creep, titanium alloy, vanadium alloy, aluminum alloy

ABSTRACT: Continuing their study of the high-temperature strength of titanium alloys, the authors investigated it in the ternary system Ti-Al-V as a function of alloy composition and structure. An isothermal section of the system at 550°C was plotted on the basis of microstructural and x-ray analyses and a determination of the properties; the regions of the \prec and β solid solutions of titanium and of the intermetallic compound Ti3Al (\prec 2 phase) are indicated (see Fig. 1). Alloys of the Ti-Al-V system along sections with constant aluminum contents of 5, 7.5, and 20% were found to have a maximum creep resistance near the boundary of the limiting solutions based on \prec Ti, β Ti, and Ti3Al; the lowest high-temperature strength is displayed by alloys from the regions (\prec 4 β) and (\prec 2+ β) with a coarse two-phase structure. Alloys from the region of the Y phase have a high creep resistance at

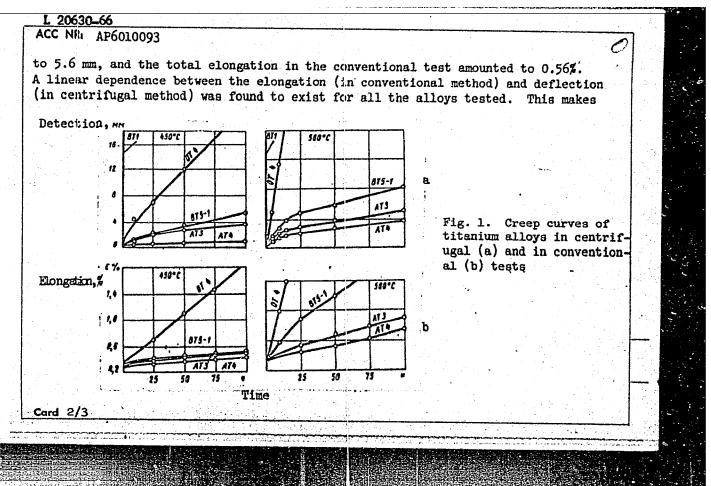
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UDC: 669.017.13

"APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R000824720011-6

SOURCE CODE: UR/0129/66/000/003/0036/0038 ENT (m)/T/EWA(d)/ENP(w)/ENP(t) 20630-66 ACC NR: AP6010093 AUTHOR: Andreyev, O. N.; Kornilov, I. I.; Martova, T. T. Institute of Metallurgy im. A. A. Baykov (Institut metallurgii) TITLE: Determination of the characteristics of heat resistance of titanium alloys SOURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 3, 1966, 36-38 TOPIC TAGS: titanium alloy, heat resistant alloy, alloy property, centrifuge test, tensile test/VT1 alloy, OT4 alloy, VT5 1 alloy, AT3 alloy, AT4 alloy, ST1 ABSTRACT: Titanium VT1 (0.3% Fe, 0.25% Si) and titanium alloys OT4 (3.5% Al, 1.78% Mn, 0.2% Fe, 0.1% Si), VVT5-1 (4.9% Al, 2.75% Sn), AT3 (3.2% Al, 0.8% Cr, 0.2% Fe, 0.1% Si), VVT5-1 (4.9% Al, 2.75% Sn), AT3 (3.2% Al, 0.8% Cr, 0.2% Fe, 0.1% Si), VVT5-1 (4.9% Al, 2.75% Sn), AT3 (3.2% Al, 0.8% Cr, 0.2% Fe, 0.1% Si), VVT5-1 (4.9% Al, 2.75% Sn), AT3 (3.2% Al, 0.8% Cr, 0.2% Cr, 0.2% Sn), AT3 (3.2% Al, 0.8% Cr, 0.2% Cr, 0.2% Sn), AT3 (3.2% Cr, 0.2% Cr, 0.3% Fe, 0.4% Si, 0.01% B) and AT4 (4.8% A1, 0.9% Cr, 0.4% Fe, 0.3% Si, 0.01% B) have been tested for creep behavior by centrifugal (Kornilov) and by conventional methods. Both tests were performed at 450 or 5000 for 100 hr under a stress 20 kg/mm². At both temperatures tested and in both test methods VT1 titanium had the highest creep rate and AT4 alloy the lowest creep rate (see Fig. 1). In stress-rupture tests at 500C under a stress of 30 kg/mm² the rupture lives were 12 hr for OT4 alloy, 30 hr for VT5-1 alloy, 210 hr for AT3 alloy, and 260 hr for AT4 alloy. Creep tests by both of the above methods were performed with STI titanium alloy of the Ti-Al-Zr-Sn system at 600C under a stress of 15 kg/mm² (alloy was annealed at 800C for 1 hr and air cooled). After 100 hr, the total deflection in the centifugal test amounted UDC: 620.172.224.226:669.295 **Card** 1/3



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I 39961-66 EUT(m)/T/EUP(w)/EUP(t)/FTT ACC NR: AP6019775

TJP(c) JG/JD

SOURCE CODE: UR/0370/66/000/003/0172/0178

AUTHOR: Kornilov, I. I. (Moscow); Shakhova, K. I. (Moscow); Budberg, P. B. (Moscow)

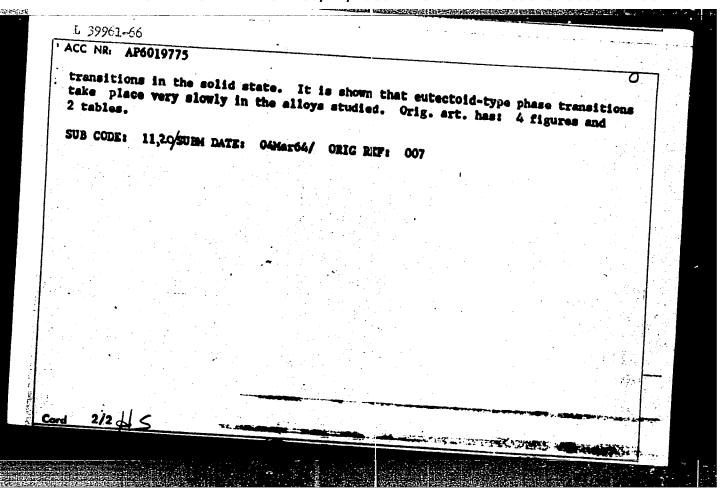
TITLE: Electrical resistance and thermal expansion of alloys of the Ti-Nb-Cr system SOURCE: AN SSSR. Izvestiya. Hetally, no. 3, 1966, 172-178 11 1 2)

TOPIC TAGS: electric resistance, thermal expansion, titanium alloy, niobium alloy,

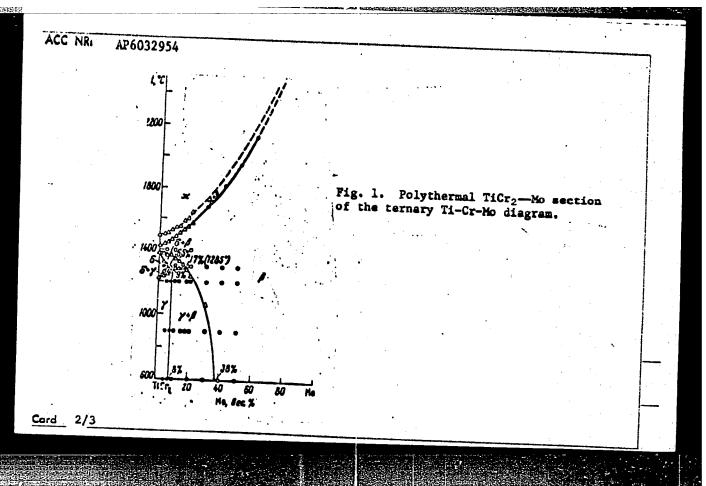
ABSTRACT: The electrical resistance of alloys of the Ti-Nb-Cr system was investigated as a function of their chemical and phase composition at room temperature and during heating to 1100°C. The thermal expansion in the 20-1100°C range was also studied. The alloys were first quenched from 1000°C and subjected to prolonged annealing. Data on the variation of the electrical resistance with the composition were found to be in good agreement with the results of microstructural and x-ray phase analyses. The electrical resistance data for the 20-1100°C range permitted the determination of the temperature boundaries of existence of the phase regions. Transition from one phase region to another was indicated by the presence of breaks in the curves of electrical resistance vs. temperature. A study of the thermal expansion of alloys during heating made it possible to establish the temperatures of

Card 1/2

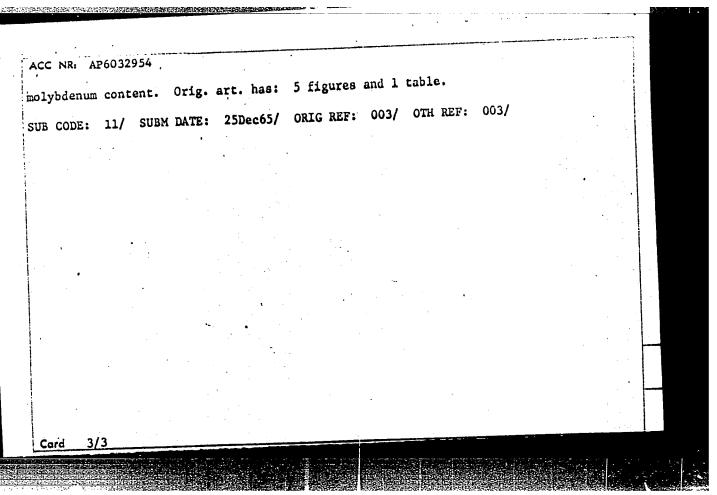
VDC: 669.295.51293126



SOURCE CODE: UR/0363/66/002/010/1878/1881 ACC NR: AP6032954 AUTHOR: Samsonova, N. N.; Budberg, P. B.; Kornilov, I. I.; Asanov, U. A. ORG: Institute of Metallurgy im. A. A. Baykov, Academy of Sciences, SSSR (Institut metallurgii Akademii nauk SSSR) TITLE: Interaction between TiCr, compound and molybdenum AN SSSR. Izvestiya. Neorganicheskiye materialy, v. 2, no. 10, 1966, 1878 to 1881 TOPIC TAGS: titanium chromium molybdenum system, titanium chromium compound, chromium compound, titanium compound, molybdenum, statum, titanium compound mo ABSTRACT: A series of chromium-titanium molybdenum alloys with compositions located on the TiCr2-No section of the ternary chromium-:itanium-molybdenum system were scull melted from 99.99%-pure components and studied by various methods of physicochemical analysis. Molybdenum was found to stabilize the β -phase ternary-molybdenumchromium-titanium solution, to raise the solidus temperature and to lower the temperature of the $\beta \rightarrow \delta + \beta \rightarrow \delta$ transformation (see Fig. 1). The microhardness of the alloys at 1300, 1200 and 600C increases with increasing molybdenum content, reaches a maximum of about 820 kg/mm² at 6.5% (1300C) or about 825 and 870 kg/mm² at 8% (1200 and 600C) molybdenum and then drops rather sharply with further increase in 546.281'76+546.77 Cord 1/3



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ACC NR. AP6032955 SOURCE CODE: UR/0363/66/002/010/1882/1886 AUTHOR: Samsonova, N. N.; Budberg, P. B.; Kornilov, I. I.; Asanov, U. A. ORG: Institute of Metallurgy im. A. A. Baykov, Academy of Sciences, SSSR (Institut TITLE: Interaction between TiCr2 compound and vanadium SOURCE: AN SSSR. Izvestiya. Neorganicheskiye materialy, v. 2, no. 10, 1966, TOPIC TAGS: titanium chromium vanadium system, titanium chromium compound, titanium compound, vanadium alloy, titanium vanadium system, titanium corromium compound, titanium compound, vanadium alloy, titanium vanadium, system chromium compound, metal chemical and sie, hadress chromium compound, metal abstract: A series of chromium-titanium-vanadium alloys with compositions located on the Titanium of the terrainium chromium alloys with compositions located on the TiCr₂-V section of the ternary chromium-titanium-vanadium diagram were levitation melted in helium atmosphere from iodide titanium, 99.99%-pure chromium and 99.75%-pure vanadium and studied by various methods of physicochemical analysis. It was found that vanadium stabilizes β-phase TiCr₂-base solid solution, raises the solidus temperature, and lowers the temperature of $\beta + \beta + \delta + \delta$ transformation (see Fig. 1). The microhardness of the alloys at 1200, 900 and 600C generally decreases with increasing vanadium content, first (in the y region) slowly, then 1/2 546.281'76+546.881

vroozht31

SOURCE CODE: UR/0000/66/000/000/0003/0015

AUTHOR: Kornilov, I. I.

ORGI none

TITIE: Development of a physico-chemical theory of heat resistance applicable to refractory metals and alloys

SOURCE: AN SSSR. Institut metallurgii. Svoystva i primeneniye zharoprochnykh splayov (Properties and application of heat resistent alloys). Hoscow, Isd-vo Hauka, 1966. 3-15

TOPIC TAGS: refractory metal, refractory alloy, heat resistance

ABSTRACT: On the basis of the physico-chemical theory, the basic factors in the strengthening of metals are: 1) formation of solid solutions; 2) reactions leading to the formation of dispersed phases; 3) formation of high melting metals as Kurnakov compounds and as compounds which crystallize out of the melt; 4) formation of solid solutions based on the refractory metals, strengthened by dispersed phases. The present article considers the solubility and dispersion mechanisms for strengthening refractory metals. The main aim of the article is a consideration of the possibility of creating new heat resistant alloys based on the refractory metals, in particular the "big four", columbium, tantalum, molybdenum, and tungsten. A table presents

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calculatapproved EGR RELEASE: 06/14/2000 CIA-RDP80-UUDIA experimental data presented, the following factors must be considered in the CIA-RDP86-00513R000824720011-6 application of solution and dispersion effects in the strengthening of alloys: 1) Use should be made of the great tendency of the transition metals, including the "oig four", toward the formation of a wide range of solid solutions. For alloys of this kind, the basic systems are tungsten-tantalum-molybdenum-columbium and tungstenmolybdenum-columbium-vanadium. 2) Using the ability of these metals to combine with light metals and metalloids (aluminum, beryllium, boron, carbon, silicon, nitrogen) to form limited solid solutions and high melting compounds (aluminides, beryllides, borides, carbides, silicides, nitrides), these metals should be used for alloying in the creation of optimum compositions for multicomponent alloys; this must be combined with solution and dispersion strengthening at high temperatures. Orig. art. has: 11 figures and 1 table.

SUB CODE: 11/ SUBM DATE: 10 Jun66/ ORIG REF: 017/ OTH REF: 012

Card 2/2

"APPROVED FOR RELEASE: 06/14/2000

EWT(m)/T/EWP(e)/EWF(t)/ETI ACC NRI AP6024395 IJP(c) AT/WH/WW/JD/JG SOURCE CODE: UR/0020/66/169/002/0343/0346 AUTHOR: Kornilov, I. I.; Glazova, V. V.; Kenina, Yo. M.

ORG: Institute of Metallurgy im. A. A. Baykov (Institut metallurgii) TITIE: Formation of the compounds Zr60 and Zr30 in the zirconium-oxygen system

SOURCE: AN SSSR. Doklady, v. 169, no. 2, 1966, 343-346

TOPIC TAGS: zirconium alloy, alloy phase diagram, annealing

ABSTRACT: Zirconium-oxygen alloys containing from 1 to 28 at. \$ oxygen were studied by physicochemical analysis, microscopic analysis, and measurements of microhardness, electrical resistance and thermal emf. Alloys quenched after annealing for 400 hr at electrical resistance and thermal emr. Alloys quenched after annealing for 400 mr at 600 °C and containing up to 8% O2 correspond to homogeneous a solid solutions. Above 8% O2, glide lines typical of decomposition of solid solutions appear. Alloys containing 15-16% O2 consist of a single phase and those with 25-26% O2 show a finea two-phase structure. Resistivity-composition curves for alloys quenched from 600 and 800° show two singular resistivity maxima at 14.5 and 25% Oz, corresponding to the stoichiometric composition of the compounds Zr60 and Zr30 respectively. A study of the temperature dependence of the electrical conductivity of these compounds (which increases with temperature) confirmed their semiconducting nature. The bonding in Zr60 is primarily covalent (with a certain fraction of ionic character). The paper Card 1/2

VDC: 546.8

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ACC NR APPROVÉD FOR RELEASE: 06/14/2000 CIA-RDP86-00513R000824720011-6

Was presented by Academician Sazhin, N. P., 27 Oct 65. Orig. art. has: 4 figures and SUB CODE:

.11/ SUBM DATE: 06Jb165/ ORIG REF: 005/ OTH REF: 008

Card 2/2

L-01305

"APPROVED FOR RELEASE: 06/14/2000 EWT(d)/EWT(m)/EWP(w)/EWP(c)/EWP(v)/T/EWP(t)/ETI/EWP(k)/EWP(h)/EWP(1) ACC NR: AP6003317 IJP(c) JD/WW/JG/WB SOURCE CODE: UR/0365/66/002/001/0025/0031 AUTHOR: Kornilov, I. I.; Vinogradov, Yu. M. ORG: Institute of Metallurgy im. A. A. Baykov (Institut metallurgii) TITLE: Use of titanium in the chemical machine building industry and its principles of alloying SOURCE: Zashchita metallov, v. 2, no. 1, 1966, 25-31 TOPIC TAGS: titanium, titanium alloy, chemical plantaquipment, corresion resistant alloy,

ABSTRACT: Titanium has a high resistance to corrosion and relatively high strength properties. This makes it an excellent structural material for producing chemical machine parts and apparatuses. At the present time only technically pure titanium (BT-1) is widely used in the industry for the production of pipes, heat-exchange apparatuses for heating electrolytes, condensars for condensation of ammonium pyrodine bases, heaters, tanks, filters, blades for centrifugal pumps for organic salts containing HCl, valve pumps, sprayers, atomizers, etc. However, titanium alloys will be more widely used in the future because BT-1 has a relatively low strength, it shows creep at room temperature, and stresses of 80% of the yielding point, as well as a low corrosion resistance in hot solutions of some acids. Some known titanium alloys

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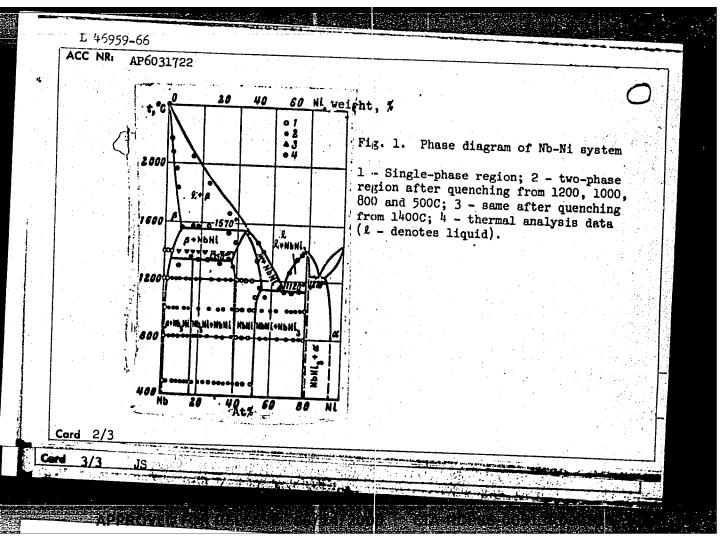
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ACC NR: APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R000824720011-6

have a higher corrosion resistance than pure titanium. Titanium alloyed with 0.2-0.3% palladium has high stability in mineral acids. The selection of alloying elements for metals, including titanium, is controlled by their reaction with the metal. A study of the metal chemistry of titanium resulted in the separation of four groups of elements in the periodic system. The elements of the first group form continuous solid solutions with titanium; the elements of the second group form limited solid solutions; the elements of the third group form ionic compounds; and the elements of the fourth group do not react with titanium. Only the first two groups are of interest for efficient alloying. The main alloying elements for the formation of corrosion- and heat resistant solubility, Oxygen, pitrogen, and hydrogen cause brittleness and dan be used only for special purposes. Alloys in the form of [32] solid solution can be made by using Mo, Nb, and V as alloying algebrate in large concentrations (>20-30g) and 7g Al Cr and Fa and V as alloying elements in large concentrations (>20-30%) and Zr, Al, Cr, and Fe in small concentrations to preserve a stable A structure of the alloy. Since there is a shortage of tantalum, it can be recommended only for special cases. The titanium points and heat resistance and can be sued as heat-resistant coatings. The ternary and more complex systems are also of interest: Ti-Mo-Nb. Ti-Mo-Zr. Ti-Cr-Cu. Ti-Zr-Sn. 1 more complex systems are also of interest: Ti-Mo-Nb, Ti-Mo-Zr, Ti-Cr-Cu, Ti-Zr-Sn, v) Ti-Pd-Cu, Ti-Mo-Pd, Ti-Mo-Cr, Ti-Cr-Pd, and others. With respect to corresion resistance interesting results can be obtained in the region of 3-solid solutions with a high concentration of molybdenum and niobium. Orig. art. has: 5 fig. and 1 table.

11,07/3/SUBM DATE: 11Mar65/ ORIG REF: 024/ OTH REF: 002

L 46959-66



ACC NR: AP7002429

SOURCE CODE: UR/0129/66/000/012/0005/0014

AUTHOR: Kornilov, I. I.

ORG: Institute of Metallurgy, AN SSSR (Institut metallurgii AN SSSR)

TITLE: Physicochemical theory of high temperature strengthening of refractory metals

SOURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 12, 1966, 5-14

TOPIC TAGS: high temperature metal, high temperature alloy, high temperature strength, melting point, exidation resistance, metal physics, dispersion strengthening, REFRACTORY ALLOY

ABSTRACT: A literature survey was made of the high temperature properties of refractory metals and alloys. Included were the metals Nb, Ta, Mo, and W and the alloying elements Hf, Rh, Ru, Os, Ir, Si, C, B, O, and N. The pure refractory metals have low strength above 0.4 T_m (T_m is the melting point) and are highly oxidizable; consequent-

ly, they are alloyed in order to produce solution or dispersion strengthening. physicochemical theories of both strengthening methods were studied. Solid solubility and local ordering were examined from the viewpoint of electronic and atomic similiarity. Data are given on the melting point, hardness, and creep strength as a function of alloying. The melting points of the refractory metals are raised substantially by selective alloying. For example, the systems Ta-W, Mo-W, Nb-Ta, Nb-Mo, Cr-Nb

UDC: 669.27'28'293'294:539.434

ACC NR: 'AP7002429

CIA-RDP86-00513R000824720011-6 **APPROVED FOR RELEASE: 06/14/2000** and V-Rh all raise their melting point as a function of alloying. The hot hardnesses of Ta-W and Nb-W, however, go through a maximum at 50% W. Besides binary and ternary systems, W-Ta-Mo-Nb and W-Ta-Mo-Nb-V are also possible as solid solution systems. The use of lighter elements (Al, B, Be, C, Si, N) in refractory metals or alloys results in intermetallic compound formation as well as solid solubility. In these cases optimum compositions must be determined to provide for solution and dispersion strengthening. The mechanism of dispersion strengthening was related to the effects of the disperse phase. For example, creep strengthening results from the distribution of the disperse phase at grain boundaries. The equilibrium solubility of carbon in tungsten is given as a function of temperature. Different refractory systems were analyzed for regions of solid solubility in order to develop rules for combining the strengthening effects of both dispersion and solution hardening. The short time tensile strength of various refractory metals and alloys was given as a function of temperature. In all cases alloying increased the strength at critical temperatures of 0.4, 0.6, and 0.8 T_m . Alloy compositions were selected near the solid solubility limits for these temperatures, thereby combining dispersion with solid solution strengthening. Orig. art. has: 6 figures, 1 table.

SUB CODE: 11/ SUBH DATE: none/ ORIG REF: 024/ OTH REF: 017

Card 2/2

APPANEROA

SOURCE CODE: UR/0020/67/172/002/0390/0393

AUTHOR: Kornilov, I. I.; Nartova, T. T.

ORG: Motallurgy Institute im. A. A. Baykov, Academy of Sciences, SSSR (Institut metallurgii Akademii nauk SSSR)

TITLE: Some regularities in the high-temperature strength of titanium alloys and types of composition vs. high-temperature strength diagrams

SOURCE: AN SSSR. Doklady, v. 172, no. 2, 1967, 390-393

TOPIC TAGS: titanium alloy, high strength alloy, solid solution

ABSTRACT: In an attempt to establish the regularities of the high-temperature strength (HTS) of titanium alloys, the following characteristics are considered on the basis of reported and experimental data; nature of the chemical reaction of Ti with other elements; formation of solid solutions and metallic compounds of Ti; solid-state phase transformations; and degree and final state of the phase equilibrium in systems based on Ti. The following conclusions were reached: (1) The change in HTS in TI systems is determined by the nature of the chemical reaction of Ti with other elements, polymorphic transformations, and types of equilibrium diagrams of Ti systems. (2) In accordance with the four basic types of equilibrium diagrams, 4 types of composition-HTS diagrams of Ti systems were established, in contrast to the three types of similar diagrams of metal systems without polymorphic transformations. Many

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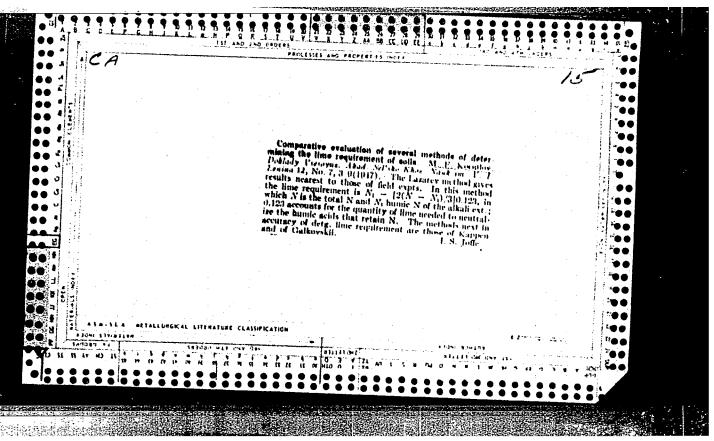
KORNILOV, K.A., kand. tekhn. nauk

Reconditioning gear wheels in repairing industrial equipment.

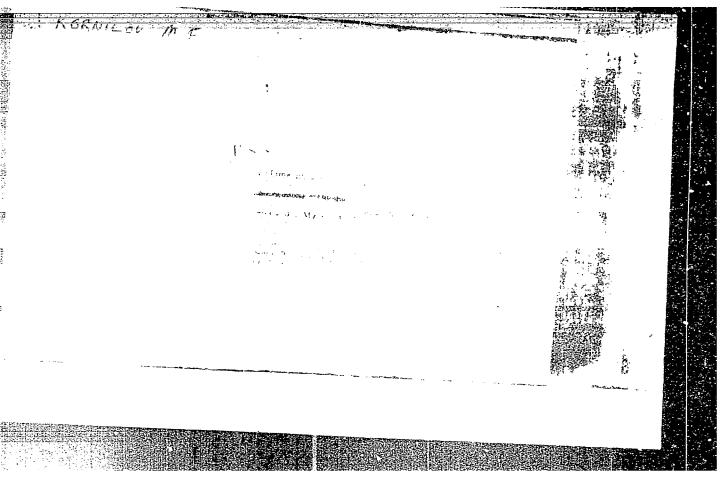
Mashinostroitel' no.5:11-12 My '65. (MIRA 18:5)

Reactivity of 1,1-dialkoxytrimethylamines. Coll Cz Chem 29
no. 3:645-651 Mr '64.

1. Institute of Organic Chemistry and Biochemistry, Czechoslavak Academy of Science Chemistry (for Arnold). 2. Kiev State University, Institute of Organic Chemistry, SSR (for Kornilov).



"APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R000824720011-6



Orni Lov, M. F.

USSR/Soil Science. Mineral Fertilizers.

I-5

I-5

Abs Jour: Referat Zh-Biol., No 6, 25 March, 1957, 22475

Author : Kornilov, M.F., Borisova, E.M., Trunina, Z.V. Inst

Title : Soil Liming and Varieties.

Orig Pub: Tr. Vses. n.-i. in-ta udobr., agrotekhn. i agropochvoved., 1955,

Abstract: Based on vegetative and field-laboratory experiments with different varieties of a number of agricultural plants conducted in the Leningrad division of the All-Union institute of fertilizers, agrotechnique and agrosoil science, it was established that varieties grown on neutral soils, rich in calcium, are more responsive to liming when grown on acid soils than varieties grown in districts further north on acid soils. These differences in behavior of varieties were mostly observed in summer wheat, barley, flax, peas, clover, and were less clearly expressed in summer

Card : 1/2

-1-

USSR/SOPPROVED FOR RELEASE: 06/14/2000 Mineral Fertilizers. CIA-RDP86-00513R000824720011-

Abs Jour: Referat Zh-Biol., No 6, 25 March, 1957, 22475

rye, vetch, buckwheat. Sensitivity to soil acidity of different oat varieties had no connection with their origin.

Card : 2/2 MASALOV, A., tekhnik-mekhanik (Ufe); HORNILOV, M., inzh.; SHIGANOV, A., (Chernigov); DUMIN, A., inzh. (Leningrad); ATUPOV, S., slesar'-instrumental'shchik (g.Kirovek, Leningradskoy oblasti); DROBYSHEVSKIY, V., insh.; VENEDIKTOV, V. (Sverdlovek)

Suggested, developed, introduced. Izobr.i rats. no.1:40-42

Ja '60. (HIRA 13:4)

SAVCHENKOV, A.F., kand.ekonomicheskikh nauk, dotsent; kornilov, M.F., doktor sel'skokhozyaystvennykh nauk; CHUBAROV, A.P., kand.sel'skokhozyaystvennykh nauk; TSITOVICH, O.B., inzhener-tekhnolog, khimik

Need in nitrogen fertilizers and their varieties in the northwestern part of the U.S.S.R. Trudy LIEI no.36:13-22 '61. (MIRA 15:1)

(Fertilizers and manures) (Nitrogen)

KORNILOV, M.F., doktor sel'skokhoz, nauk (Leningrad)

Needs of the agriculture of the northwestern areas of the U.S.S.R. in nitrogen fertilizers. Trudy LIEI no.37:7-13

161. (MIRA 18:4)

KCRNILOV, M.F., doktor sel'skdkhozyaystvennykh nauk; KHCDASEVICH, B.G.;
CHURKIN, K.G.

Using town construction and industrial waste for the fertilization of fields. Zemledelie 24 no.10:62-68
0 '62.

(MRRA 15:11)

1. Severe-Zapadnyy nauchno-issledovatel'skiy institut sel'skogo khozyaystva (for Kornikov). 2. Leningradskiy sel'skokhozyaystvennyy institut (for Khodasevich).
3. Ural'skiy nauchno-issledovatel'skiy institut sel'skogo khozyaystve (for Churkin).

(Fertilizers and mamures)
(Waste products)

ASTAKHOV, I.I., glav. red.; ANSIN, A.N., red.; IVANOV, D.A., red.; KORNILOV, M.F., doktor sel'khoz. nauk, red.; KONYUKHOV, V.N., kand. sel'khoz. nauk, red.; MARKITANTOVA, A.V., uchenyy sekretar', red.; SAPOZHNIKOV, N.A., red.; DMITRIYEV, N.N., red.

[Science in the service of agricultural production; collection of scientific and technical information] Nauka - sel'skokhoziai-stvennomu proizvodstvu; sbornik nauchno-tekhnicheskoi informatsii. Leningrad, Lenizdat, 1964. 143 p. (MIRA 17:3)

1. Leningrad. Severo-zapadnyy nauchno-issledovatel'skiy institut sel'skogo khozyaystva.

YERMOLAYEVA, Antonina Nikitichna; KORNILOV, M.F., doktor selkhoz. nauk, nauchn. red.; TOLOCHINSKAYA, B.M., red.; KRYUCHKOVSKIY, S.A., red.

[Chemistry in agriculture; index of recommended literature for compulsory education in agrochemistry] Khimiia v sel'-skom khoziaistve; rekomendatel'nyi ukazatel' literatury v pomoshch' agrokhimicheskomu vseobuchu. Leningrad, 1964. 51 p. (MIRA 17:11)
1. Leningrad. Publichnaya biblioteka.

KOBYL'SKAYA, M.V.; KORNILOVA M.F.; SEMENOV, S.S.; PYSHKINA, M.I.;
PUS TOVALOVA Ye.K.; KUZNETSOVA, O.A.; Prinimali uchastiye;
KSENOPONTOVA, tekhnik; ATZENBERG, Z.M., tekhnik; LOBANOVA, E.M.,
tekhnik

Using said asphalt for the preparation of superphosphate
phosphorous fertiliser. Trudy VNIIT no.12:119-129 '63.

(MIRA 18:11)

YURK, Yu.Yu., doktor geol.-miner. nauk, prof., otv. red.;
GOROSHNIKOV, B.I.[Horoshnykov, B.I.], kand. geol.miner. nauk, red.; KARASIK, M.A.[Karasyk, M.A.], kand.
geol.-miner. nauk, red.; KORNILOV, M.O.[Kornylov, M.O.],
kand. geol.-miner. nauk, red.; LEBEDINSKIY, V.I.
[Lebedyns'kyi, V.I.], kand. geol.-miner. nauk, red.;
SHTUL'MAN, I.F., red.; DAKHNO, Yu.B., tekhn. red.

[Mineralogy and geochemistry of the southeastern part of the Ukrainian S.S.R.] Mineralogiia i geokhimiia pivdennoskhidnoi chastyny URSR. Kyiv, Vyd-vo AN Ukr.RSR, 1963. 148 p. (MIRA 17:1)

1. Akademiya nauk URSR, Kiev.

Followelane from the crust of weathering of ferruginous quartities of the Korsak Mogila deposit. Dop, AN URSR no.8:1111-1114 '63. (MIRA 16:10) 1. Institut mineral'nykh resursov AN UkrSSR. Predstavleno akademikom AN UkrSSR N.P. Semenenko [Semenenko, M.P.]. (Korsak Mogila mountain—Psilomelane)

Ionogenic addition of halogens to bis-methylene bases of nitrogencontaining heterocycles. Zhur.ob.khim. 31 no.5:1699-1705 My '61.

(MIRA 14:5)

1. Kiyevskiy gosudarattennyy universitet.

(Polymethylene compounds)

KORNILOV, M.Yu.; ARNOL'D, Z.

Activity of dimethylformamide acetals. Zhur.ob.khim. 34 no.2:700-701
F '64. (MIRA 17:3)

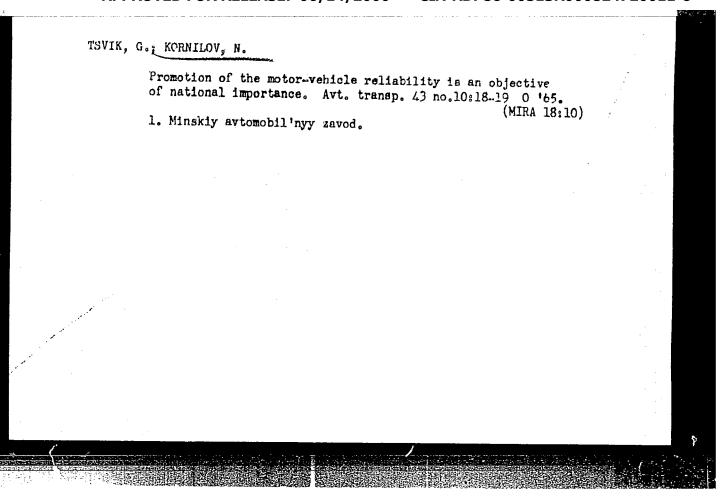
1. Institut organicheskoy khimii 1 biolkhimii Akademiii nauk Chekhoslovatskoy Sotsialksticheskoy Respubliki, Praga, i Kiyevskiy gosudarstvennyy universitet.

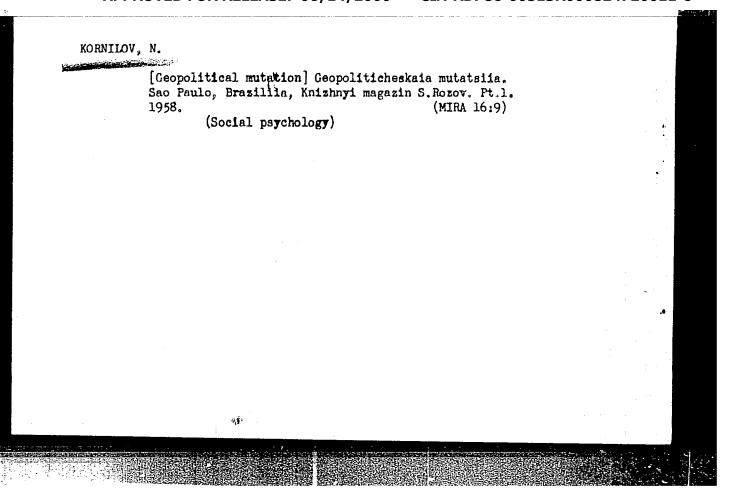
KIPRIANOV, A.I.; KORNILOV, M.Yu.

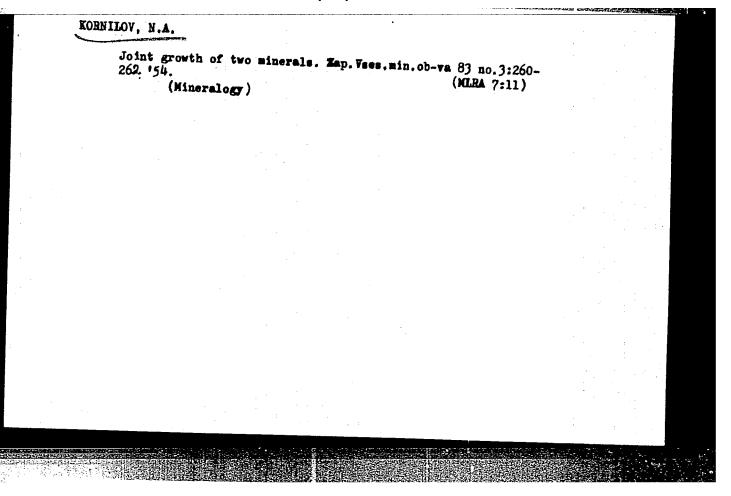
Tonogenic addition of halogens to bis-methylene bases of nitrogen heterocycles. Part 2. Zhur.ob.khim. 34 no.1:77-82 Ja '64.

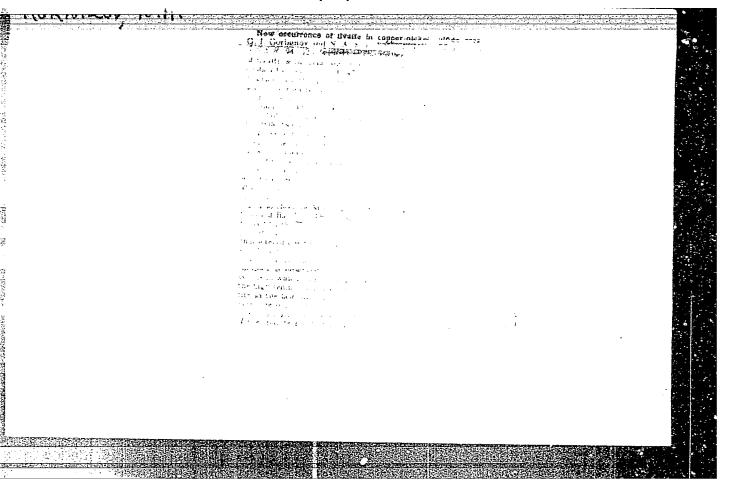
1. Kiyevskiy gosudarstvennyy universitet.

(MIRA 17:3)









Core metasomatosis in the Pechenga copper and nickel sulfide deposits. Izv. Ear. i Kol'.fil.AN SSSR no.4:20-31 '58.

1. Laboratoriya mineralogii i geokhimii Kol'skogo filiala AN SSSR.

(Pechenga District—Ore deposits)

(Metasomatism)

AUTHORS:

Ivanova, V. P., Kornilov, N. A.

20-119-1-42/52

TITLE:

Asbestiform (Transverse Fibrous) Chlorite From a Copper-Nickel Deposit (Asbestovidnyy (poperechnovoloknistyy)

khlorit iz medno-nikelevogo mestorozhdeniya)

PERIODICAL:

Doklady Akademii Nauk SSSR, 1958, Vol. 119, Nr 1,

pp. 154-157 (USSR)

ABSTRACT:

Scaly aggregate-forms are characteristic of the minerals of the chlorite-group; asbestiform ones are unknown. In similar layered chrysolite and endellionitz asbestiform aggregates form a union of individual tubes the walls of which consist of several atomic layers (Reference 1). Therefore the investigation of individual fibers in this chlorite is of interest. It was found in the form of black, small veins in a hydrothermally changed schist at the contact with epigenetic copper-nickel grains of ore which are genetically connected with ultrabasic rocks. The mineral can easily be separated in individual small columns or needles which glimmer through dark-green at the edges. Its hardness is 2-2,5 (figure 1). The microscopic struc-

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APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R000824720011-Asbestiform (Transverse Fibrous) Chlorite From a 20-119-1-42/52 Copper-Nickel Deposit

> ture is described in detail. The chemical composition (table 1) permits to classify the chlorite with the mage nesic group; it is placed near the boundary with ferriferous-magnesic chlorites (Reference 2). A crystallochemical formula after recalculation to 18 oxygen atoms is given. Beside the elements mentioned in table 1 Ni, Co, V, Cu, Zn and traces of Be, Ca, Zr and Sr were determined by spectral analysis. The debye crystallogram is very similar to those of scaly chlorites. The comparison of the lattice-parameters, calculated from the interplanar spacings (table 2) was performed. The calculated parameters as compared to the theoretical ones show a considerab= ly higher quantity of the parameter c. The differential curves of heating were obtained according to the method described in reference 4. For the asbestiform chlorite, ground to a different degree of comminution, they are given in figure 3. These curves are dependent on the degree of comminution (References 5, 6). The causes of the stronger projection of the exothermic peak following

Card 2/4

Asbestiform (Transverse Fibrous) Chlorite From a Copper-Nickel Deposit

20-119-1-42/52

the two endothermic effects in the case of a finer commi= nution of the chlorite deserve a special investigation and discussion, which the authors intend to perform. In order to be able finally to judge on the shape of the elementary particles which form the finest fibers of chlorite they were investigated in the electron-microscope. The particles proved to be scaly. The assumption on the tubular structure of the asbestiform are thus confirmed. At the same time the optical properties of the asbestiform chlorite essentially differ from those of scaly chlorite. According to the type of pleochroism and the position of the axes of the indicatrix the asbestiform chlorite is close to the usual negative chlorites. It differs from the latter by the extreme-ly large angle 2V (-130°). A similar distortion of the optical properties is characteristic of the minerals of the serpentine-group. There are 3 figures, 2 tables and 6 references, 4 of which are Soviet.

Card 3/4

Some observations on the contact of effusive diabases of the Pachenga series. Izv. Kar. i Kol'. fil. AN SSSR no.1:33-39
159. (MIRA 12:9)

1.Geologicheskiy institut Kol'skogo filiala AN SSSR.

(Kola Peninsula--Diabase)

KORNILOV, N.A.; DENISOV, A.P.

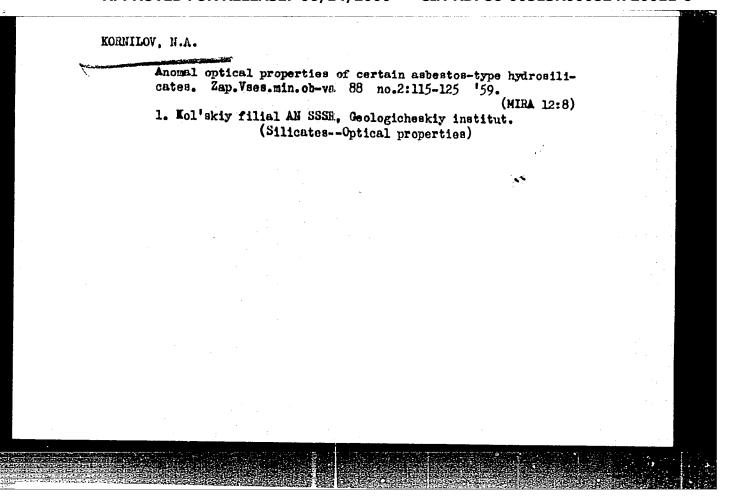
Composition and conditions governing the formation of pyrrhotite and troilite in the Pechenga copper-nickel deposits. Isv.Kar. i Kol'.fil.AN SSSR no.4:24-33 '59. (MIRA 13:5)

1. Geologicheskiy institut Kol'skogo filiala AN SSSR. (Pechenga region--Pyrrhotite)

KORNILOV, N.A.

Large meteer ever the Kela Peninsula. Prireda 48 no.6:113 Je
'59. (MIRA 12:5)

1.Kel'skiy filial AM SSSR, Kirevsk.
(Neteers)



KORNILOV, N. A., Cand Geol-Min Sci -- (diss) "Characteristics of hydrothermal wall rocks and ore metasomatosis in the Fechengskiye Copper-Nickel Deposits. (Kol'skiy Peninsula)." Leningrad, 1960. 26 pp; (Ministry of Higher and Secondary Specialist Education RSFSR, Leningrad Orders of Lenin and of Labor Red Banner Mining Inst im G. V. Plekhanov); 200 copies; price not given; printed on duplicating machine; list of author's work on pp 25-26; (KL, 24-60, 120)

| | iy filial AN SSSR Soyusnogo mineral orites) | , Geologicheskiy institu | t. Deystvitel'nvv | |
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Mineralogy of serpentines. Zap. Vses.min.ob-va 90 no.5:535-548
161. (MIRA 14:10)

1. Kol'skiy filial AN SSSR, Geologicheskiy institut. (Serpentine)

KORNILOV, N.A.

Quartz from sulfide copper-nickel ores of Pechenga. Geol.rud. mestorozh. no.4:123-126 J1-Ag '62. (MIRA 15:8)

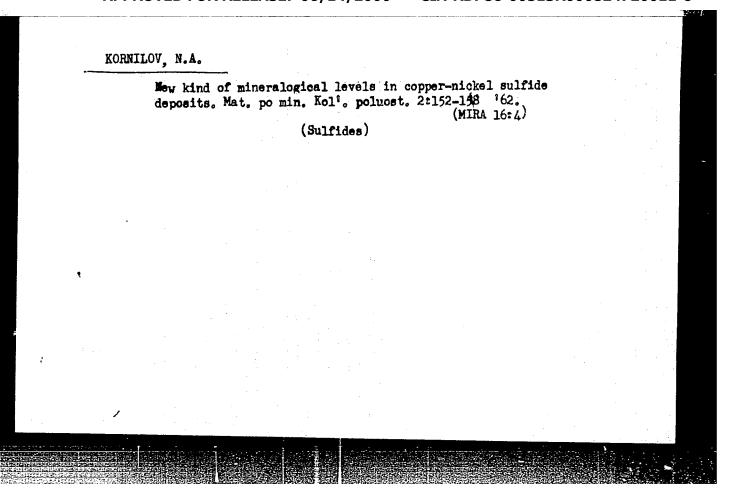
KORNILOV, N.A.

Sulfide olivinites and harzburgites of the Allarechensk nickelbearing intrusive (Kola Perinsula). Dokl. AN SSSR 146 no.1:199-202 S 1 2. (MIRA 15:9)

1. Institut mineral'nykh resursov AN USSR. Predstavleno akademikom V.S. Sobolevym.

akademikom V.S. Sobolevym.
(Kola Peninsula—Olivinites)
(Kola Peninsula—Harzburgite)

| 1. Institut mineral nykh resursov AN SSSR, Simteropol . (Shells—Analysis) |
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KORNILOV, N.A.

Redoposition of impregnated sulfides in the process of forming sulfide cuprous nickel deposits. Dokl. AN SSSR 152 no.2:396-399 S '63. (MIRA 16:11)

1. Institut mineral'nykh resursov AN UkrSSR. Predstavleno akademikom D.S.Korzhinskim.

Natural sulfide-silicate liquation. Mat. po min. Kol'.
poluost. 3:100-106 '62, (MIRA 17:3)

IVANOVA, V.P.; KORNILOV, N.A.

Effect of the degree of the dispersion of minerals of the scrpentinite and chlorite group on their thermal characteristics. Trudy VSEGEI 96:187-201 '63. (MIRA 17:9)

YURK, Yu.Yu.; KORNILOV, N.A.; KIRICHENKO, O.N.; LEBEDEV, Yu.S.

Outlines of the Cimmerian iron ore basin in the southern part the U.S.S.R. Dokl. AN SSSR. 154 no.2:355-358 Ja'64.

(MTRA 17:2)

1. Institut mineral'nykh resursov AN UkrSSR. Predstavleno akademikom D.I. Shcherbakovym.

Strontium in the Kimmeridge from re deposits of the Azov and Black Ses Basin. Gookhimits no.2.241-245 F '65.

(MIRA 18:6)

1. Inātitut mineral'nykh resursov Gosudarstvennogo geologicheskogo komitete SSSR, Simferopol'.

Tavrovskiy, V.A.; IVANOV, D.U.; ECENTICOV, N.A.

Pirst results of reacclimatizing sables in the southern and eastern regions of Yakutia. Trudy Inst.biol.IAPAN SSSR no.4:
3-49 158. (NIRA 11:11)

(Takutia—Sables)

ACC NR. AM6015327 Monograph UR/ Onoshko, YUriy Anatol'yevich; Gittsigrat, Ernest Ernestovich; Kornilov, Nikita Ivanovich: Kokovkin, Viktor Sergeyevich Drilling holes with diamond bits (Bureniye skvazhin almaznymi dolotami) Leningrad, Izd-vo "Nedra", 1965. 307 p. illus., biblio. 2000 copies printed. TOPIC TAGS: drilling, diamond bit drilling, drilling tool, drilling equipment, geologic survey, geologic prospecting, diamond specification PURPOSE AND COVERAGE: This book is intended for geological engineering personnel and for students of geological survey tekhnikuns. It may also serve as textbook for improving the qualifications of drilling teams. The book reviews the most important properties of diamonds used for drilling geological survey holes in rocks of various hardness. Designs of equipment and tools used in drilling mond bits and methods and procedures applied to drill test holes are discussed in detail. TABLE OF CONTENTS [abridged]: Foreword -- 3 Introduction -- 4 Card 1/2

ACC NRI AM6015327 Ch. I. Daimonds and their application in the industry -- 9 Ch. II. Drill bits with small-size diamonds -- 39 Ch. III. Equipment for drilling with diamonds -- 107 Drilling technology - 161 Ch. IV. Problems of drilling rocks with small-size diamond bits -- 270 Ch. V. Ch. VI. Safety precautions in drilling works -- 283 Ch. VII. Documentation and records kept in drilling with diamond bits -- 289 Appendix -- 292 References -- 304 SUB CODE: SUBM DATE: 06Dec65/ ORIG REF: 032/ OTH REF: Card

Diamond drilling is a most important potential for increasing drilling cutput. Razved. 1 okh. nedr 31 no.2:21-24 P 165.

(MIEA 18:3)

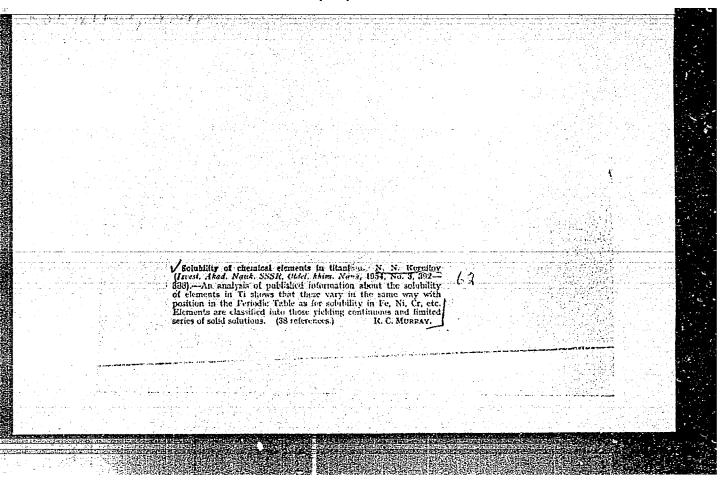
1. Vsesoyuznyy nauchno-issledovateliskiy institut metodiki i tekhniki razvedki Gosudarstvennogo geologichoskogo komiteta SSSR (for Isayev). 2. Gosudarstvennyy geologicheskiy komitet SSSR (for Kornilov).

CIA-RDP86-00513R000824720011-6 "APPROVED FOR RELEASE: 06/14/2000

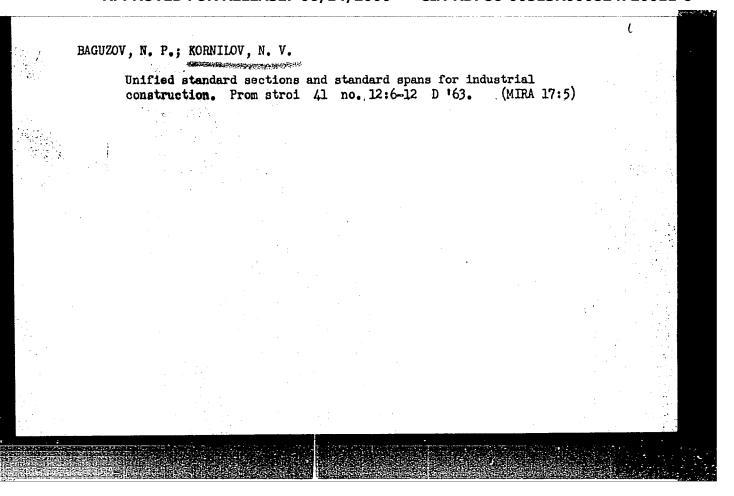
KORNILOV, N.I.; KUROCHKIN, P.N.

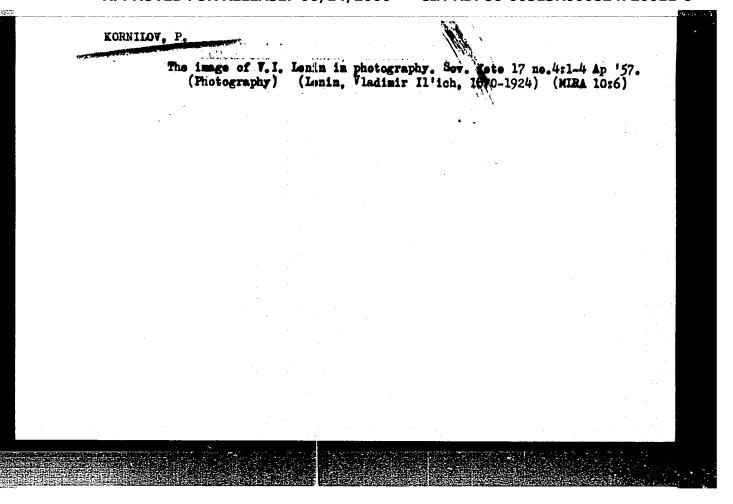
Using low-quality diamonds in drill bltm. Razved. I okh. nodr 30 no.9:23-25 5 164. (MIRA 17:12)

- Gosudarstvennyy geologicheskiy komitet SSSR (for Kormilov).
 Vsesoyuznyy nauchno-issledovatel'skiy institut metodiki i tekhniki razvedki Gosudarstvennogo geologicheskogo komiteta SSSR (for Kurochkin).



Continuous assembly line for front axles of cars and equipment for attaching springs. Obm.tekh.opyt.na avt.transp. no.3:49-48 '60. (MIRA 13:7) (Antomobiles—Maintenance and mpair)





APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R000824720011-6"

VYDRIN, Vladimir Nikolayevich, doktor tekhn. nauk; SITNIKOV, Leonid Leonidovich, inzh.; KORNILOV, Petr Vasil'yevich, inzh.; SVET, Ye.B., red.

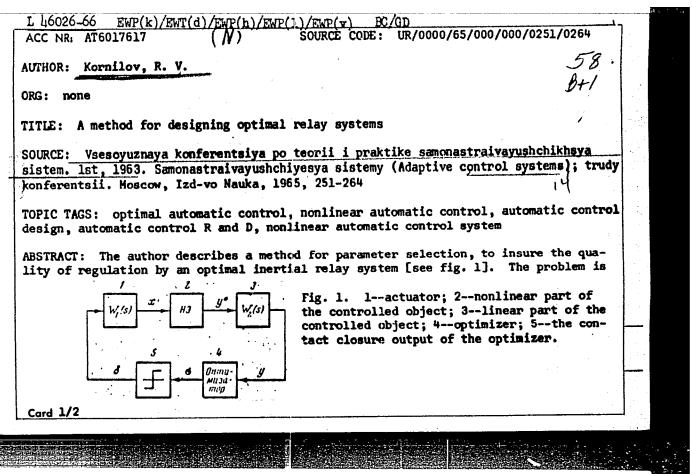
[Strength of rolling-mill rolls] Stoikost' prokatnykh valkov. Cheliabinsk, Cheliabinskoe knizhnoe izd-vo, 1964. 70 p. (MIRA 17:8)

TETAL RAUM, S.I., prof.; KORNILOV, R.A., nauchnyy sotrudnik (Kiyev)

Portable ergometer-ergograph, Vrach.delo nc.11:1211-1212 M '57.

1. Chlen-korrespondent AM USSR
(DYMANOMETER) (ERGOGRAPH)

KORNILOV, R. A.: Master Med Sci (diss) -- "Investigation of the static-dynamics of the body under normal conditions and in certain pathological states of the support-motor apparatus". Kiev, 1959. 19 pp (Kiev Order of Labor Red Banner Med Inst im Acad A. A. Bogomolets), 200 copies (KL, No 8, 1959, 138)



L 46026-66

ACC NR: AT6017617

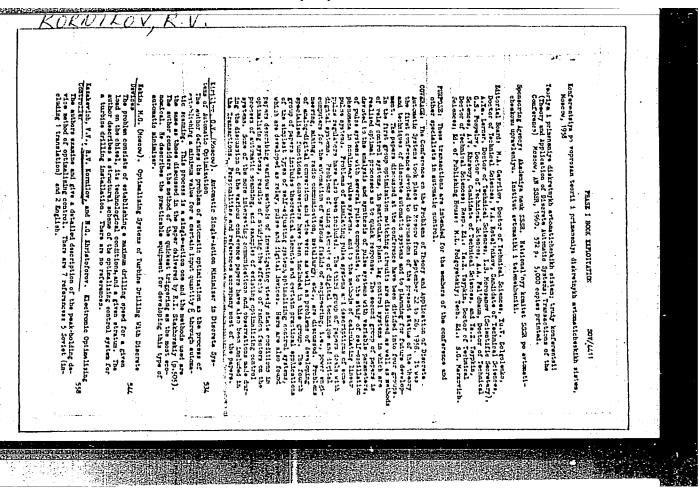
to find for given transfer functions of blocks 1, 2 and 3 a set of parameters for the optimizer which would insure the desired performance. Two performance aspects are chosen as the design criteria: the minimum search time (to generate an output) during which given search losses are not to be exceeded, and minimum search losses. The author selected two approaches to the solution of this problem, both of which are thoroughly explained and analyzed. The first method is a point transformation, resulting in a set of design formulas, graphs and rules; the second, following from the first, is a method for numerical solution using an analog computer. The analysis is based on the assumption that the nonlinear static response characteristic of the block (3) can be made linear on a piecewise basis to any desired degree of approximation. This approach is particularly suitable when the response of the controlled object cannot be described by a parabolic function. Orig. art. has: 36 formulas, 9 figures.

SUB CODE: 13/ SUBM DATE: 22Nov65/ ORIG REF: 007

Card 2/2 9/

EWT(d)/EWP(v)/EWP(k)/EWP(h)/EWP(1)GD/BC 46030-66 SOURCE CODE: UR/0000/65/000/000/0265/0277 ACC NR: AT6017618 37 AUTHOR: Putsillo, V. P.; Bobrov, Yu. I.; Kornilov, R. V. B+1 ORG: none TITLE: Methods of constructing single channel automatic optimizers for inertial processes SOURCE: Vsesoyuznaya konferentsiya po teorii i praktike samonastraivayushchikhsya sistem. 1st, 1963. Samonastraivayushchiyesya sistemy (Adaptive control systems); trudy konferentsii. Moscow, Izd-vo Nauka, 1965, 265-277 TOPIC TAGS: optimization, optimal control, extremal control, NONLINEAR CONTROL SYSTEML ABSTRACT: Two methods of synthesizing a controller for a nonlinear, inertial, extremal control system are presented. The synthesis is performed by analyzing the output of the system by a phase plane diagram. The first method establishes the control law by evaluating the first order derivative of the output, while the second method utilizes the second order derivative as well. The second method is supposed to improve the stability of the system. The control law is expressed as a logical binary algorithm and schemes composed of logical elements to perform the control functions are proposed. The second method proposed by the authors is criticized by V. V. Kazakevich, whose work is referred to in this paper. His conclusion is that the perform-Card 1/2

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27639 S/194/61/000/002/028/039 D216/D302

AUTHORS:

Kazakevich, V.V, Kornilov, R.V. and Khristoforov,

N.G.

TITLE:

Electronic extremum controller

PERIODICAL:

Referativnyy zhurnal. Avtomatika i radioelektronika, no. 2, 1961, 39, abstract 2 V316 (V sb. Teoriya i primeneniye diskretn. avtomat. sistem, M., AN SSSR,

1960, 558-569)

TEXT: In an extremum controller operating with storage of the extremum, the fundamental disturbance is the fast monotonically disappearing extremum characteristic. For the stabilization of the position of the controlling device it becomes then advantageous to use a commutator which periodically reverses the speed of the machine. The presence of inertia or delay in the load influences the steady-state of a system with such a controller. If in a load without inertia in its steady-state positive and negative increments

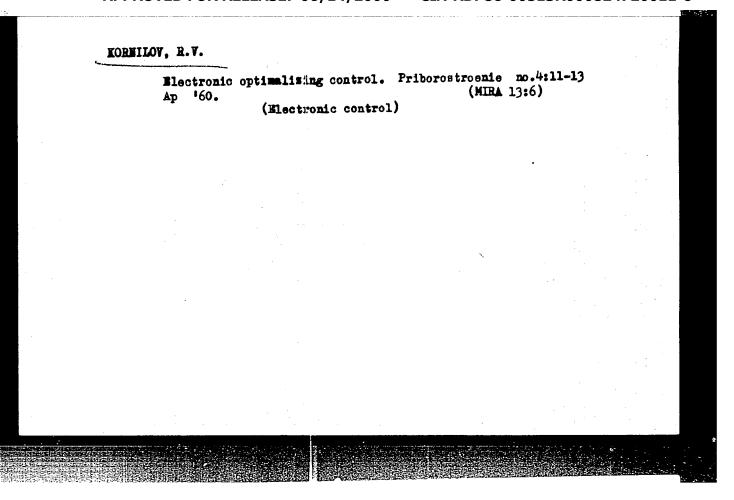
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Electronic extremum controller

alternate, then in the load with inertia after a few positive increments, the same number of negative increments will follow (the characteristic is said to be symmetrical). The bloc-diagram of extremum controller consists of a signum-relay determining the sign of the increment, a commutator and output device. The operation of the signum-relay and of the commutator are synchronized. The extremum controller has been tried on a model of the load. 7 references.

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\$/569/61/006/000/003/008 D201/D303

AUTHORS:

Putsillo, V. P., Petrov, V. V., Kornilov, R. V. and

Volodin, Ye. Ye. (USSR)

TITLE:

Principles of design of one class of extremum control

systems for the automation of production processes

SOURCE:

International Federation of Automatic Control. 1st Congress, Moscow, 1960. Trudy. v. 6. Avtomatizatsiya proisvodstvennykh protsessov; khimiya, neftepererabotka,

teploenergetika, yadernaya energetika, metallurgiya.

Moscow, 1961, 356-366

TEXT: The authors describe an extremum control system designed for controlling processes with large time constants in the linear sections. This extremum control system is the easiest to design and is based on the method of forced reversals or hunting with "memorizing" the extremum. When the controller is switched in, the controlling element starts to move in any direction, thus producing changes in the controlled quantity y. The controlling signal is ac-

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Principles of design ...

tually the sign of a finite increment: $\Delta = \text{sign}(y_i - y_{i-1})$. If the maximum is sought, then at $\Delta > 0$ the motion is allowed for, but at Δ < 0 the drive of the controlling element is reversed. The blocdiagram of an extremum controller is given. It has the following main units: 1) Input unit (IU), which determines the sign of the increment of controlled quantity by comparing its current magnitudes with those previously stored; 2) commutator unit, providing the forced reversal of the system, excluding the consecutive signals of one sign and controlling the IU; 3) output unit (0U) for producing a signal with enough power for controlling the drive of the controller; 4) the switching-off unit (SO) which disconnects the controller when extremum is meached and relative of the controller. the controller when extremum is reached and makes a reversed connection, if no disturbance changing the position of extremum is acting upon the system; 5) control velocity regulator (CVR) providing a wide range of regulation of the motor (output stage) velocity. The circuit diagram of the arrangement is given. The controller has been experimentally tried with a high-temperature tunnel furnace. The controller made it possible to control the fur-

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Principles of design ...

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nace temperature within 3 - 4°C (nominal operating temperature was 1600 - 1650°C). The maximum deviation during the transitional unstable state did not exceed 9 - 12°C. At the same time the air consumption was down by 20%. The results obtained were in agreement with the requirements. V. V. Petrov (USSR) took part in the discussion and acknowledges the help of Professor V. V. Kazakevich and of Engineer A. L. Malyy in designing the first model of the extremum control of the tunnel furnace. There are 5 figures and 6 references: 5 Soviet-bloc and 1 non-Soviet-bloc. The reference to the English-language publication reads as follows: C. S. Draper, L i J. T. Principles of optimalizing control, ASME, 1951.

Card 3/3

RIPOVITERIT, M.D.; FORMILOV, R.V.

Maing optimalizing controllers in a continuous furnace.

Filmonostroenie no.1125-7 E '61. (MRA M.'10)

(Formostat)

(Thermostat)

"APPROVED FOR RELEASE: 06/14/2000

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S/103/63/024/002/007/020 D201/0308

AUTHORS:

Bobrov, Yu. I., Kornilov, R.V. and Putsillo, V.P.

(Moscow)

TITLE :

Determination of the control law of an optimizer,

taking into account the inertness of the object

PERIODICAL:

Avtomatika i telemekhanika, v. 24, no. 2, 1963,

183-191 1

The authors analyze the on-off extremum control systems, in which the controlled object is represented by a first order factor, a non-linear element with one extremum and has an inactive zone. From the analysis of the system's motion in the phase plane the structure of the optimizer controller is derived and it is shown that, for the above class of systems, a stable search for optimum is achieved by introducing the second derivative: this is done bearing in mind that, for objects with an inactive zone and low speed of the output stage, the signal from the second derivative may be commensurable with the inactive zone. The synthesis of the con-Card 1/2

Determination of the control law ...

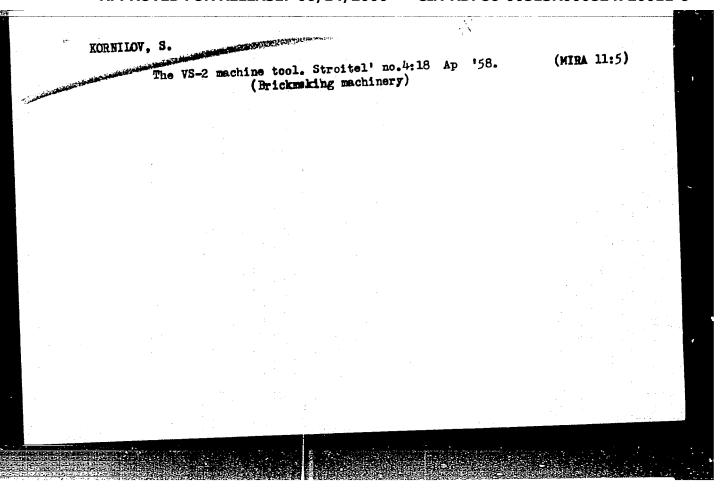
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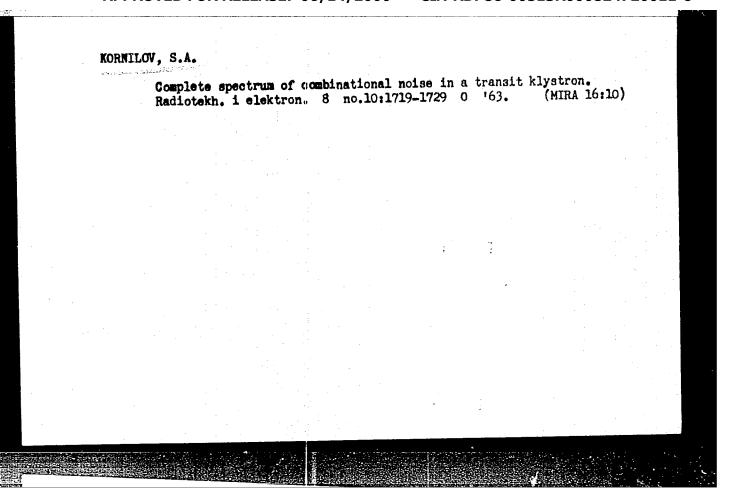
trol law was used for selecting the functional diagram of the optimizer. The first derivative signal is differentiated and a signal proportional to the second derivative, is applied to the summing element, to which the compensating constant signal is also applied. If the output from the summing element is less than - £, where £ is the inactive zone of the relay, a signal is applied to a logic circuit, which then transmits a pulse from the timing generator. This output is then applied to a trigger circuit, which reverses the direction of the output stage. A model of the device, with polarized relays as sensing elements, operated in full agreement with the theory. There are 7 figures.

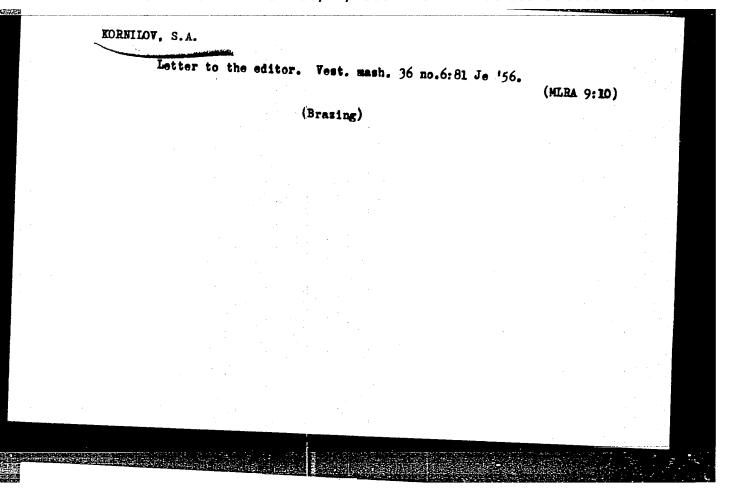
SUBMITTED:

March 27, 1962

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SOV/112-58-3-5047

Translation from: Referativnyy zhurnal. Elektrotekhnika, 1958, Nr 3, p 241 (USSR)

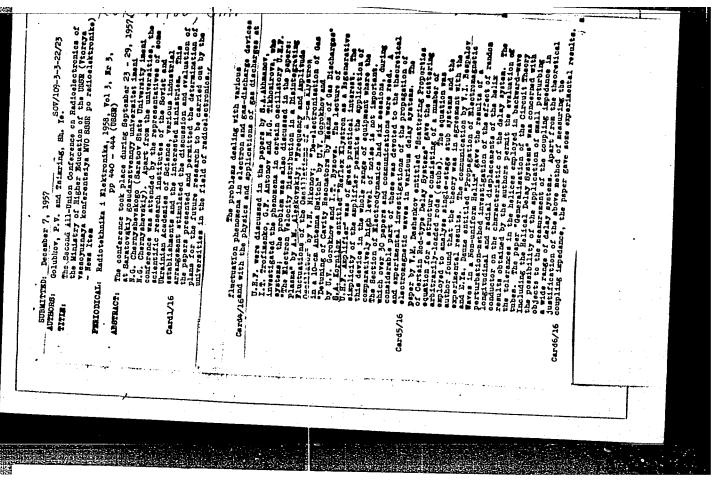
AUTHOR: Kornilov, S. A.

TITLE: SHF Amplification by Means of an Underexcited Reflex Klystron (Usileniye SVCh-kolebaniy s pomoshch'yu nedovozbuzhdennogo otrazhatel'nogo

PERIODICAL: Nauchno-tekhn. inform. byul. Leningr. politekhn. in-t, 1957,

ABSTRACT: An underexcited reflex klystron is used as a regenerative amplifier. Fundamental parameters of the amplifier are determined. Experiments in the 3×10^9 - and 10×10^9 -cps bands have confirmed the theoretical conclusions.

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SOV-109-3-4-9/28

AUTHOR: Kornilov, S. A.

TITLE: Frequency Division in Transit-Time Klystrons with Three Grid Systems (Deleniye chastoty v proletnom klistrone s tremya zazorami)

PERIODICAL: Radiotekhnika i Elektronika, 1958, Vol 3, Nr 4, pp 522-529 (USSR)

ABSTRACT: The system considered (see Fig.1) consists of a singleresonator oscillator stage and a modulating grid system. For
the purpose of analysis, the output resonator system can be
represented by an equivalent R, L and C circuit, which can
be described by the differential equation:

$$\frac{d^2 U_3}{dt^2} + 2\delta \frac{dU_3}{dt} - 2\delta R \frac{di_H}{dt} + \omega_0^2 U_3 = 0, \qquad (1)$$

where i_H is the current induced at the output grids, U_3 is the voltage at the third grids, U_1 is the modulating voltage, having a frequency $N\omega$, δ = 1/2 RC and ω_0 = $1/\sqrt{LC}$. Eq.(1) can be written (see Ref.1) in the form of Card 1/4

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Frequency Division in Transit-Time Klystrons with Three Grid

Eq.(2), whose right-hand portion is written as Eq.(2a). If it is assumed that the velocity modulation of the electron beam in the first resonator is small, the convection current i2 _, appearing at the second grid system can be represented by Eq. (4), in which Io is the beam current, to is the instant of the appearance of the electrons at the second grids, XO is the bunching parameter defined by β_1 is the coefficient of electron where interaction in the first grid system, 0 is the transit angle of the electrons in the first transit space, a is the amplitude of the modulating signal and $\tilde{U_0}$ is the DC potential of the beam. It is shown that for N=2 the induction current at the third grid system can be expressed

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Frequency Division in Transit-Time Klystrons with Three Grid Systems by Eq.(7) in which

$$X = \sqrt{X_a^2 + X_b^2}$$
 and $tg \varphi = \frac{X_b}{X_a}$

and X_a and X_b are defined by Eqs.(5). On the basis of Eq.(7), it is possible to describe the transient processes of the system by Eqs.(8) in which X is the bunching parameter and ϕ is the phase. When the transit angle θ_2 for the second grid system is an optimum, Eqs.(8) can be written as Eqs.(9). In the steady state, Eqs.(9) are written as Eqs.(10) from which it follows that the bunching parameter of the system can be expressed by:

$$x^{2} = 8 \left\{ 1 - \frac{1 - \sqrt{1 - \left(1 - \frac{m^{2}}{4}\right) \left(1 + 4Q^{2}\eta^{2}\right)}}{\gamma \left(1 - \frac{m^{2}}{4}\right)} \right\}$$
 (11)

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BOV-109-3-4-9/28

Frequency Division in Transit-Time Klystrons with Three Grid Systems $m = 2 \mathcal{J}_1(X_0)$, $\eta = (\omega - \omega_0)/2\omega$ and $Q = \omega/2\delta$ Eq.(11) is used to determine the synchronisation bandwidth of the system and to construct a number of graphs (see Figs. 5, 6 and 7). From the above analysis it is concluded that a triple resonator klystron can be used as a reliable frequency divider. The characteristics of such a divider (the presence of an excitation threshold and the shape of the resonant curves) are similar to those of an electron tube frequency divider. In the case of a two-to-one frequency division the klystron gives a synchronisation bandwidth equal to that of the output resonator. 7 figures and 3 Soviet and 1 English references.

SUBMITTED: December 10, 1956.

1. Klystrons—Analysis 2. Klystrons—Applications 3. Frequency dividers--Equipment 884. Differential equations--Applications

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69267 SOV/112-59-17-37505

Translation from: Referativnyy zhurnal. Elektrotekhnika, 1959, Nr 17, pp 235-236 (USSR)

AUTHORS:

Kornilov, S.A., Nelepets, V.V. ----

TITLE:

Experimental Characteristics of the Reflex Clystron as a Regenerative Microwave Amplifier

PERIODICAL: Nauchno-tekhn. inform. byul. Leningr. politekhn. in-t, 1958, Nr 5, pp 40-47

ABSTRACT:

Results of a study of operating characteristics of regenerative VHF-amplifiers on reflex clystrons of 3 cm and 10 cm band are cited. The measurements in the 10 cm band were carried out on clystrons with an outside resonator; the regulation of the feedback factor was performed by the change of the beam current. The measurements in the 3 cm band were performed on clystrons with inside resonators; a special device for reduction of the loaded circuit quality was used. The obtained values of the amplification coefficient and graphs of dependence of the pass-band of the amplifier on the amplification coefficient are supplied. The maximum attainable amplification for clystrons of both types is approximately 30 - 35 db. On the clystron of the 3 cm band it was possible to obtain a pass-band of approximately 10 Mc at an amplification of 10 - 15 db. The sensitivity of clystrons of both types was

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